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**PATENT APPLICATION
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EYE SAFE HIGH POWER FIBRE LASER

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EYE SAFE HIGH POWER FIBRE LASER**Cross Reference to Related Applications**

The present application is a U.S. National Stage filing of Patent Cooperation Treaty ("PCT") application serial number PCT/GB2004/003265, filed 28 July 2004, which in turn claims priority to United Kingdom (Great Britain) Patent Application Serial Numbers GB 0317604.7, filed 28 July 2003, GB 0404594.4, filed 02 March 2004, and GB 0406765.8, filed 26 March 2004, all of which are incorporated by reference herein in their entirety.

Field of Invention

This invention relates to an apparatus for providing optical radiation. The invention has particular relevance for welding, drilling and cutting applications using lasers in factory environments in which light scatter from ceilings and other surfaces represents a safety hazard, and for low heat generation in high-power fibre lasers.

Background to the Invention

Fibre lasers are increasingly being used for material processing applications such as welding, cutting and marking. Their advantages include high efficiency, robustness and high beam quality. Examples include femtosecond lasers for multiphoton processing such as the imaging of biological tissues, Q-switched lasers for machining applications, and high-power continuous-wave lasers.

Traditional lasers used for material processing applications predominate at around 1.06 μ m and longer wavelengths such as provided by a carbon dioxide laser (10.6 μ m). These lasers are being supplemented by fibre lasers operating at around 1.06 μ m. Light scattered from the work piece when using such fibre lasers is a problem because the scatter is at wavelengths at which the retina of the eye can be easily damaged.

It is desirable to have eye safe wavelengths for scatter light considerations. This means wavelengths longer than 1400nm, and preferably between 1500nm and 2500nm. Erbium is a suitable dopant for fibre lasers outputting in the 1550nm wavelength window. Erbium doped fibres can be pumped at a variety of wavelengths, including by high-power diode lasers operating between 915nm and

1 980nm. Unfortunately, the erbium doped fibre is not very efficient when pumped at
2 915nm and this leads to undesirable heat generation within the erbium doped fibre.

3 It is also desirable to improve the thermal management of fibre lasers so as to
4 reduce the problem of heat generation within a high power fibre laser. The main
5 source of heat generation is due to the quantum defect (ie the difference in photon
6 energy between the pump and the laser photons).

7 It is also preferable to use an optical fibre material that has good heat
8 resistance, low loss properties, and that can be fusion spliced.

9 Laser diodes have reduced life if they are pulsed and this therefore limits the
10 life of high power fibre lasers that are pumped by pulsed laser diodes. A solution is
11 to accept diode failures and to provide redundancy. Commercial systems available
12 today can use between 10% and 20% more laser diodes than would otherwise be
13 required if the laser diodes were more reliable. It would be an advantage to improve
14 the reliability of pulsed fibre lasers that are pumped by laser diodes.

15 An aim of the present invention is to provide an apparatus for providing optical
16 radiation that reduces at least one of the above aforementioned problems.

17 18 **Summary of the Invention**

19 According to a non-limiting embodiment of the present invention, there is
20 provided apparatus for providing optical radiation comprising a pump source and at
21 least one first amplifying waveguide, CHARACTERISED IN THAT the first amplifying
22 waveguide emits optical radiation in excess of 1400nm when pumped by the pump
23 source.

24 The pump source may include a plurality of laser diodes and at least one
25 second amplifying waveguide, wherein the first amplifying waveguide is pumped by
26 the second amplifying waveguide, and the second amplifying waveguide is pumped
27 by the laser diodes, the apparatus being characterised in that the second amplifying
28 waveguide is configured to improve the beam quality of radiation emitted by the laser
29 diodes. The beam quality of the radiation emitted by the laser diodes can be
30 measured in terms of its beam parameter product (here defined as half divergence
31 angle, half focussed spot radius). The product of the numerical aperture and $1/e^2$
32 guided beam radius (approximately the core radius for a waveguide having a core) of
33 the second amplifying waveguide should be less than the beam parameter product
34 of the radiation supplied from the laser diodes.

1 The pump source may include at least one multimode beam combiner for
2 combining optical radiation emitted by the laser diodes.

3 The apparatus may include at least one first beam combiner for combining
4 optical radiation emitted by the second amplifying waveguides.

5 The first amplifying waveguide may comprise a first optical fibre.

6 The first optical fibre may comprise a region containing a first rare-earth
7 dopant. The first rare earth dopant may be selected from the group comprising
8 erbium, holmium and thulium. The first rare earth dopant may be co-doped with
9 ytterbium. The apparatus may be such that the first rare-earth dopant is pumped
10 substantially at the peak of its absorption band.

11 The first optical fibre may comprise a core and a cladding. The first optical
12 fibre may be single mode or multi mode. The first optical fibre may comprise a
13 plurality of cores.

14 The second amplifying waveguide may comprise a second optical fibre. The
15 second optical fibre may comprise a region containing a second rare-earth dopant.
16 The second optical fibre may comprise a core and a cladding. The second optical
17 fibre may comprise a grating written into at least one of the core and the cladding.
18 The second optical fibre may be single mode or multi mode. The second optical
19 fibre may comprise a plurality of cores.

20 The apparatus may include means to change the wavelength of radiation
21 emitted by the second amplifying waveguide. The means may be a wavelength
22 tuneable reflector, an optical switch, a source of optical radiation, or a tuneable
23 grating. The tuneable grating may be thermally tuned, or tuned by an actuator.

24 The apparatus may be configured such that the optical radiation emitted by
25 the first amplifying waveguide has a higher brightness when the second amplifying
26 optical fibre emits at a first wavelength. This is a particularly advantageous
27 implementation of the invention in that it is useful for modulating high-power fibre
28 lasers that are pumped by a plurality of laser diodes. By high power, it is meant a
29 fibre laser that emits greater than 10W of optical radiation, and preferably greater
30 than 100W. The invention is particularly advantageous for high power fibre lasers
31 that emit between 1kW and 10kW of optical radiation. Instead of switching the laser
32 diodes on and off, the fibre laser can be controlled with a lower power signal.
33 Advantages include increasing the life of the laser diodes, and removing the need for
34 switching electrical power. Additionally, as will be described herein, the present

invention allows distributed thermal management and shorter, more powerful lasers – particularly at so-called “eye-safe” wavelengths.

The apparatus may be such that the pump source supplies pump radiation for in-band pumping the first amplifying waveguide. The pump wavelength and the wavelength of the optical radiation may both be between 1400nm and 2500nm.

The pump source may comprise a broad stripe laser diode.

The optical radiation may be coupled to a scanner. The apparatus may include a controller for synchronizing the optical radiation with the scanner.

The apparatus may be in the form of an amplifier, a laser, a master oscillator power amplifier, a Q-switched laser, a source of amplified spontaneous emission, or a continuous wave laser.

The apparatus may be in the form of a laser for material processing.

Brief Description of the Drawings

Embodiments of the invention will now be described solely by way of example and with reference to the accompanying drawings in which:

Figure 1 shows an apparatus for providing optical radiation according to the present invention;

Figure 2 and 3 show cladding pumped optical fibres;

Figure 4 shows apparatus comprising a plurality of first fibre pump modules;

Figure 5 shows apparatus which is end pumped;

Figure 6 shows apparatus containing a plurality of second fibre pump modules;

Figure 7 shows apparatus in the form of a master oscillator power amplifier;

Figure 8 shows apparatus in the form of a continuous wave laser;

Figure 9 shows apparatus comprising a plurality of second amplifiers;

Figure 10 shows apparatus including an actuator;

Figure 11 shows apparatus including a source of optical radiation; and

Figure 12 shows apparatus in the form of a laser for material processing.

Detailed Description of Preferred Embodiments of the Invention

With reference to Figure 1, there is shown apparatus 10 for providing optical radiation 15 comprising a pump source 19 and at least one first amplifying

1 waveguide 1, characterised in that the first amplifying waveguide 1 emits optical
2 radiation 15 in excess of 1400nm when pumped by the pump source 19.

3 Figure 1 shows the pump source 19 comprising a plurality of laser diodes 3
4 and a plurality of second amplifying waveguides 2. The first amplifying waveguide 1
5 is pumped by the second amplifying waveguides 2. The second amplifying
6 waveguides 2 are pumped by the laser diodes 3. The second amplifying
7 waveguides 2 are configured to improve the beam quality of radiation emitted by the
8 laser diodes 3. The beam quality of the radiation emitted by the laser diodes 3 can
9 be measured in terms of its beam parameter product (here defined as half
10 divergence angle, half focussed spot radius). The product of the numerical aperture
11 and $1/e^2$ guided beam radius (approximately the core radius for a waveguide having
12 a core) of the second amplifying waveguide 2 should be less than the beam
13 parameter product of the radiation supplied from the laser diodes 3.

14 The first amplifying waveguide 1 is preferably a cladding pumped optical fibre
15 such as the first amplifying fibre 20 shown in Figure 2. The first amplifying fibre 20
16 comprises a first core 21 and a first cladding 22, and first rare earth dopant 23 in at
17 least one of the first core 21 and the first cladding 22. Also shown is a coating 24
18 which may be a glass or a polymer. The refractive index of the coating 24 is
19 preferably less than the refractive index of the first cladding 22.

20 The second amplifying waveguide 2 is preferably a cladding pumped optical
21 fibre such as the second amplifying fibre 30 shown in Figure 3. The second
22 amplifying fibre 30 comprises a second core 31 and a second cladding 32, and
23 second rare earth dopant 33 in at least one of the second core 31 and the second
24 cladding 32. For circular fibres, the product of the radius 34 of the second cladding
25 32 and the numerical aperture 35 derived from the refractive index difference
26 between the second cladding 32 and the coating 24 should be greater than the beam
27 parameter product of the radiation supplied to the second amplifying fibre 30 from
28 the laser diodes 3. This is to ensure that the second amplifying fibre 30 can guide
29 the pump radiation efficiently. The product of the radius 36 of the second core 31
30 and the numerical aperture 37 derived from the refractive index difference between
31 the second core 31 and the second cladding 32 should be greater than the beam
32 parameter product of the radiation supplied to the second amplifying fibre 30 from
33 the laser diodes 3. This is to increase the brightness of the pump radiation that will
34 be supplied to the first amplifying waveguide 1 in Figure 1 from the second

1 amplifying waveguide 2. Modifications to these principles will be required for fibres
2 with non-circular cores and claddings, or to fibres which do not have a core, but
3 which guide using longitudinally extending holes (micro-structured fibres).

4 The first and second claddings 22, 32 can be circular or non-circular. The first
5 and second claddings 22, 32 can contain flats machined on their surface in order to
6 form a D-shape. The first and second claddings 22, 32 can be solid or may
7 comprise longitudinally extending holes. Longitudinally extending holes are
8 advantageous for guiding pump radiation without the pump radiation "seeing" the
9 coating 24. This therefore has thermal dissipation advantages in that the coating 24
10 may be a metal coating, which would otherwise attenuate the pump radiation as it
11 propagates along the cladding. The metal coating may be soldered to a heat sink.

12 Referring to Figure 1, the first amplifying waveguide 1 may be part of a fibre 8
13 that contains the first amplifying waveguide 1 (preferably in the form of the first
14 amplifying fibre 20) and at least one pump fibre 7 surrounded by a common
15 coating 9. The first amplifying waveguide 1 and the pump fibre 7 are in optical
16 contact along at least a portion of their length. This is only one example of a
17 cladding-pumped fibre and that the invention can be used with other forms of
18 cladding-pumped fibres that are described in the literature.

19 The invention is particularly useful for application in high power fibre lasers
20 emitting optical radiation 15 between 1500nm and 2500nm. For example, if the first
21 rare earth dopant 23 is erbium and the pump diodes 3 emit optical radiation at
22 976nm, then the conventional solution for pumping the first amplifying fibre 20 would
23 be to combine the optical radiation from the laser diodes 3 and couple the radiation
24 into the first amplifying fibre 20. This approach is limited by the poor beam quality
25 provided by the output of laser diodes. The conventional approach leads to large
26 diameters of the first cladding 21 (for example 500um to 5mm) and inefficient
27 absorption of the pump radiation by the first amplifying fibre 20 which leads to
28 undesirable heat generation. The inclusion of the intermediary stage involving the
29 second amplifying fibre 30 permits brightness conversion. Thus the multimoded
30 pump radiation emitted by the diode lasers 3 is converted to pump radiation having a
31 higher beam quality in order to pump the first amplifying fibre 20. Thus for example,
32 the second rare-earth dopant 33 may be erbium codoped with ytterbium, and pump
33 radiation at a wavelength of 910nm to 980nm can be used to cladding pump the
34 second amplifying fibre 30 whose second core 31 may be single mode (or multimode

1 or contain a plurality of single mode or multimode cores) and be configured to emit
2 radiation at 1530nm (or 1460nm to 1550nm). This is a convenient wavelength for in-
3 band pumping the first rare earth dopant 23 (in this case erbium). It is then possible
4 to reduce the cross-section of the first cladding 22 to smaller dimensions than would
5 otherwise be possible, resulting in increased absorption and thus shorter fibre length.
6 Advantageously, the invention also provides a method of distributing the thermal
7 dissipation in several stages. This is particularly advantageous for providing high
8 power (100W to 10kW) optical radiation 15 in the eye safe 1500 to 1650 wavelength
9 window as the efficiency of cladding pumped erbium doped amplifiers can be
10 relatively low (eg 25% to 30%) if pumped from 915nm. The advantages combine to
11 give an apparatus that is very advantageous for material processing applications
12 where the control of thermal dissipation near the work piece and the eye safe
13 wavelengths provide excellent safety advantages over existing systems.

14 Referring to Figure 1, the apparatus 10 may include first reflectors 4 and
15 second reflectors 5 in order to form a laser cavity in the second amplifying
16 waveguide 2. The first and second reflectors 4, 5 may be mirrors, reflectors,
17 gratings, or fibre Bragg gratings. If the second rare-earth dopant 33 is erbium
18 codoped with ytterbium, then it is advantageous to separate out the photosensitive
19 region (typically doped with germinia) which is used to form the fibre Bragg grating
20 from the region doped with the second rare-earth dopant 33 (which would require
21 phosphorus co-doping). The second amplifying waveguide 2 may comprise a single
22 core 31 which may be single moded or multi moded. Alternatively, the second
23 amplifying waveguide 2 may comprise a plurality of cores 31 which may be single
24 moded or multi moded. A fibre amplifying optical fibre comprising multiple single
25 mode cores is advantageous because it facilitates the writing of single-mode or
26 multi-mode fibre Bragg gratings in each of the cores. Multiple cores containing fibre
27 Bragg gratings offer a route towards high efficiency and shorter fibre lengths. Writing
28 of the single mode fibre Bragg gratings is further facilitated by arranging the cores 21
29 linearly across the fibre's cross-section. The cores 21 can be spaced sufficiently far
30 apart so as not to cause interference effects.

31 Also shown in Figure 1 are first beam combiners 11 which combine the pump
32 radiation from the laser diodes 3. The first beam combiners 11 can be multi-mode
33 beam combiners that can incorporate tapers in order to couple from an input fibre 12
34 to the second amplifying waveguide 2 (preferably in the form of the second

1 amplifying fibre 30). Beam combiners are available which can couple the power
2 from three, seven, nineteen or higher numbers of fibres. Alternatively, the first beam
3 combiners 11 can comprise lenses, splices between fibres of different diameters, or
4 etched fibre sections.

5 The pumps 3, first beam combiner 11, second amplifying fibre 30, and first
6 and second reflectors 4, 5 comprise a first fibre pump module 17 as shown in
7 Figure 1.

8 Figure 4 shows apparatus 40 comprising second fibre pump modules 43
9 which comprise a plurality of the first fibre pump modules 17 whose outputs are
10 combined in a second beam combiner 41. The second fibre pump modules 43 are
11 used to pump the first amplifying waveguide 1 (preferably in the form of the first
12 amplifying fibre 20). The second beam combiners 41 may combine the outputs of
13 between 2 and 64 first fibre pump modules 17, with 3, 7, and 19 being preferred
14 numbers.

15 The pump diodes 3 may be single emitters which are currently available at
16 power levels of 5W to 10W. If the first and second beam combiners 11, 41 each
17 combine 19 inputs, then continuous wave output power levels up to 3.6kW multiplied
18 by the efficiency of the second amplifying fibre 30 are achievable. Assuming 25%
19 efficiency (for erbium pumped pumped at 915nm and emitting at 1532nm), the first
20 amplifying fibre 20 shown in Figure 4 can be pumped by up to 4kW of pump energy
21 with the majority of the wasted energy being dissipated in the first fibre pump
22 modules 17. The invention thus provides a method of achieving eye-safe laser
23 radiation at high powers with the benefit of distributing the thermal heat load to avoid
24 concentrating inefficiencies in the final stage. It is also believed that such a double
25 pumping arrangement is more efficient than using 1480nm pump diodes to pump the
26 first amplifying waveguide 1 directly. This efficiency advantage may be overcome if
27 1480 to 1550 pump diodes can be made more efficient.

28 Figure 5 shows apparatus in which a pump source 51 pumps the first
29 amplifying fibre 20 in an end-pumped configuration. The pump source 51 can be the
30 first or second fibre pump source 17, 43.

31 Figure 6 shows apparatus comprising a plurality of the fibre pump sources 51
32 coupled into the first amplifying fibre 20 by side couplers 62. The side couplers can
33 take many forms known in the art for cladding pumping fibre amplifiers and lasers
34 including the fibre arrangement 9 shown in Figures 1 and 4.

Figure 7 shows apparatus in the form of a master oscillator power amplifier (MOPA) 70 comprising a seed source 71 and first and second amplifiers 72, 73. Also shown is an optional optical isolator 74 for preventing undesirable feedback into the first amplifier 72. The first amplifier 72 can be a conventional optical amplifier, the apparatus 10 shown in Figure 1, the apparatus 40 shown in Figure 4, or apparatus described with reference to Figures 10 and 11. The first and second amplifiers 72, 73 may comprise cascaded gain media. The second amplifier 73 can be the apparatus 10 shown in Figure 1, the apparatus 40 of Figure 4, or apparatus described with reference to Figures 10 and 11. The seed source 71 can be a laser diode, a fibre laser, a Q-switched laser, a gas laser, or a solid-state laser. The seed source 71 is selected such that the first amplifying waveguides 1 in the first and second amplifiers 72, 73 provide amplification when pumped by the pump diodes 3.

Figure 8 shows apparatus in the form of a continuous wave laser 80 comprising the first and second amplifiers 72, 73, and first and second reflectors 81, 82. The first and second reflectors 81, 82 can be mirrors, reflectors, gratings, or fibre Bragg gratings.

Figure 9 shows apparatus that comprises a plurality of second amplifiers 73 driven from a common seed source 91 via beam splitter 95. The beam splitter 95 can comprise optical fibre couplers. The seed source 91 can be a laser, a laser diode, a fibre source, or a fibre laser. The output radiation 15 of the second amplifiers 73 can be combined together in the beam combiner 92 to provide the output 93. The beam combiner can utilize coherent beam combining or incoherent beam combining. The beam combiner 92 may comprise a plurality of lenses, mirrors and/or prisms.

Although the description pertaining to eye safety and the selection of the first rare earth dopant 23 concentrate on erbium, the first rare earth dopant 23 may be selected from the group comprising erbium, holmium and thulium. The rare earth dopant 23 may be co-doped with ytterbium. This has been found to be advantageous for erbium ytterbium doping when utilizing in-band pumping even though the ytterbium has no spectroscopic function. The ytterbium appears to increase the efficiency of the erbium, possibly by improving its solubility. Ytterbium codoping also appears to avoid other deleterious effects such as clustering which can give rise to up conversion.

1 The invention is also useful for other wavelength regimes. Thus the first and
2 second rare earth dopants 23, 33 can be selected from the group erbium, ytterbium,
3 holmium, terbium, and neodymium.

4 The laser diodes 3 can be broad stripe laser diodes. Alternatively or in
5 addition, at least some of the laser diodes 3 can be diode bars or diode stacks. The
6 first beam combiner 11 can be a lens or a fused taper coupler such as described in
7 United States patent US 5864644, which is hereby incorporated herein by reference.
8 The pump fibre 7 may be a high numerical aperture multimode optical fibre.

9 The apparatus 10 is in the form of a source of amplified spontaneous
10 emission or an amplifier. The apparatus 10 can be configured as a laser which may
11 be pulsed, modulated, Q-switched, or continuous wave.

12 Figure 10 shows apparatus in which the wavelength of radiation emitted by
13 the second amplifying waveguide 2 can be changed by an actuator 101 attached to
14 the second reflector 5 in first fibre pump module 102. The actuator 101 and second
15 reflector 5 combination is a tuneable wavelength reflector which can be a grating that
16 is thermally tuned or tuned by application of stress and/or strain. Thus for example,
17 the second amplifying fibre 30 can be doped with ErYb and emit optical radiation
18 normally at around 1 μ m. If the first and second reflectors 4, 5 are selected to reflect
19 in the wavelength range 1460nm to 1550nm, then by tuning the reflectivity of at least
20 one of them (by wavelength and/or amplitude) such that both the first and second
21 reflectors 4, 5 reflect at the same wavelength in the range 1460nm to 1550nm, the
22 second amplifying fibre 30 can be turned into a laser emitting at 1460 to 1550nm. If
23 the first amplifying fibre 20 is doped with Er then the erbium can be pumped in a
24 manner that is controllable by the actuator 101. The second amplifying fibre 102 can
25 contain reflectors 105, 106, which may be mirrors, gratings or fibre gratings
26 configured such that apparatus 100 lases when pumped in the wavelength range
27 1460nm to 1550nm. This can be achieved if the reflectors 105, 106 reflect at longer
28 wavelengths, say at 1560nm.

29 An alternative means for changing the wavelength of radiation emitted by the
30 second amplifying waveguide 2 is shown in Figure 11. In Figure 11, a source of
31 radiation 111 is included in each first fibre pump module 112. The source of
32 radiation 111 can be a laser that is controlled by application of a signal.
33 Advantageously, the second amplifying waveguide 2 may contain ErYb dopant and

1 the first fibre pump module 112 may be configured by first and second reflectors 4, 5
2 to emit radiation at 1090nm. Preferably the first and second reflectors 4, 5 would
3 have relatively low reflectivity (0.1% to 10%) in order to clamp the gain. This can be
4 advantageous to prevent spontaneous pulses from damaging the apparatus.
5 Injection of radiation in the wavelength range 1500nm to 1550nm by the source of
6 radiation 111 (which may be a laser diode or fibre laser) of sufficient power level will
7 cause the second amplifying fibre 30 to amplify the radiation and thus pump the first
8 amplifying fibre 20 (preferably doped with erbium) in order to emit the desired optical
9 radiation 15. Thus control of the source of radiation 111 can be used to modulate
10 the optical radiation 15 which is beneficial for many high power laser applications
11 because it avoids modulating the laser diodes 3.

12 Other means for changing the wavelength of radiation emitted by the second
13 amplifying waveguide 2 include a wavelength tuneable reflector and an optical
14 switch.

15 In general the second amplifying fibre 30 in Figures 10 and 11 can be
16 designed such that it can emit optical radiation at a first wavelength λ_1 or a second
17 wavelength λ_2 in response to a signal (not shown). The first amplifying fibre 20 is
18 then designed such that the optical radiation 15 has a higher brightness when the
19 second amplifying optical fibre 1 emits at the first wavelength λ_1 than the second
20 wavelength λ_2 . This is a particularly advantageous implementation of the invention,
21 useful for modulating high-power fibre lasers that are pumped by a plurality of laser
22 diodes. By high power, it is meant a fibre laser that emits greater than 10W or
23 optical radiation, and preferably greater than 100W. The invention is particularly
24 advantageous for high power fibre lasers that emit between 1kW and 10kW of optical
25 radiation. Instead of switching the laser diodes on and off, the fibre laser can be
26 controlled with a lower power signal. Advantages include increasing the life of the
27 laser diodes, and removing the need for switching electrical power. Additionally, as
28 described in this specification, the invention allows distributed thermal management
29 and shorter, more powerful lasers – particularly at so-called “eye-safe” wavelengths.

30 Referring back to Figure 1, the pump source 19 can be a pump diode or a
31 module comprising a plurality of pump diodes that emit at a pump wavelength λ_p .
32 The first amplifying waveguide 1 may be the first amplifying fibre 20, and the pump
33 source 19 selected to in-band pump the first rare earth dopant 23. The first rare

1 earth dopant 23 may be erbium. Erbium doped amplifiers as used in
2 telecommunication systems are generally pumped by laser diodes having
3 wavelengths of either 980nm or 1480nm. High power amplifiers and lasers
4 containing erbium are generally pumped at 980nm, or at 915nm if the fibre is co-
5 doped with ytterbium. However these wavelengths are not ideal for high-power
6 lasers including high-power lasers for material processing applications. In-band
7 pumping erbium means that the pump wavelength λ_p should be between 1400nm
8 and 1600nm.

9 Preferably the pump wavelength λ_p should be near the peak absorption of the
10 first rare-earth dopant 23, for erbium this being at around 1530nm, and certainly
11 within a range of 1525nm to 1535nm. In order to minimize heat dissipation in the
12 first amplifying waveguide 1, the optical radiation 15 can have a signal wavelength
13 λ_s (not shown) close (within 15nm, but preferably within 5nm) to the pump
14 wavelength λ_p . More typically, it is desirable to optimise pump absorption and
15 efficiency, and to achieve this with reasonably low thermal dissipation. Pump
16 absorption is optimised by pumping at the peak of the absorption band of the rare-
17 earth dopant within the glass matrix. Thus for a phosphosilicate core doped with
18 erbium, the pump wavelength λ_p can be 1530nm to 1540nm (preferably 1535nm)
19 with the signal wavelength λ_s at a wavelength between 1560nm and 1650nm. More
20 generally the pump wavelength λ_p can be between 1460nm and 1540nm, and the
21 signal wavelength λ_s greater than the pump wavelength λ_p by more than 25nm, and
22 preferably by more than 45nm. Similar design rules will apply to fibres doped with
23 other dopants including rare-earth dopants, although the precise wavelengths will be
24 different. Advantages include efficient pump absorption (which reduces the length of
25 the optical amplifying waveguide 1), reduction in thermal effects within the optical
26 amplifying waveguide 1 by reducing the wavelength difference between pump
27 wavelength λ_p and signal wavelength λ_s , and that both the pump wavelength λ_p and
28 the signal wavelength λ_s can be configured at eye safe wavelengths. The
29 advantages combine to give an apparatus 10 that is very suited for materials
30 processing applications where the control of thermal dissipation near the work piece
31 and the eye safe wavelengths provide excellent safety advantages over existing
32 systems.

1 Although the above description concentrates on erbium, the first rare earth
2 dopant 23 may be selected from the group comprising erbium, holmium and thulium.
3 By appropriate selection of these rare earth dopants, it is possible to set the pump
4 and signal wavelengths within the range 1400nm to 2500nm. This feature is
5 advantageous for eye safety, especially in the event of a fibre break in a factory
6 environment.

7 Figure 12 shows apparatus in the form of a laser 120 for materials processing
8 120, which apparatus comprises a laser 121 emitting optical radiation 15 which is
9 coupled to a scanner 123. The laser 121 can be the laser shown in Figures 5 to 11.
10 The laser 121 can comprise the double pumping arrangements that include the
11 second amplifying waveguide 2, or the arrangements with direct diode pumping of
12 the first amplifying waveguide 1. Preferably, the laser 121 uses the apparatus
13 shown in Figures 10 and 11. The scanner 123 directs the optical radiation 15 to a
14 work piece 124. An optional controller 125 is shown for synchronizing the laser 121
15 with the scanner 123. Synchronization can be achieved by direct diode modulation,
16 modulation of the seed source in a MOPA configuration, or by Q-switching. The
17 controller 125 may be computer controlled. The apparatus is useful for materials
18 processing applications with short (10 to 50ns) high-energy (0.1mJ to 1mJ) pulses at
19 eye safe wavelengths, and with the low thermal heat generation advantages that can
20 be achieved with in-band pumping.

21 It is to be appreciated that the embodiments of the invention described above
22 with reference to the accompanying drawings have been given by way of example
23 only and that modifications and additional components may be provided to enhance
24 performance.

25 The present invention extends to the above-mentioned features taken in
26 isolation or in any combination.